

$$N_c = p_d$$

$$N_c e^{-\beta(\varepsilon_c - \mu)} = N_d \frac{1}{1 + 2e^{-\beta(\varepsilon_d - \mu)}} \quad ; \quad N_c = \frac{1}{4} \left(\frac{2m^* k_B T}{\pi \hbar^2} \right)^{3/2}$$

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vaj*

$$e^{\beta \mu} = \frac{1}{4} e^{\beta \varepsilon_d} \left[-1 + \sqrt{1 + \frac{8N_d}{N_c} e^{\beta(\varepsilon_c - \varepsilon_d)}} \right]$$

a) $T = 2 K \quad \frac{8N_d}{N_c} e^{\beta(\varepsilon_c - \varepsilon_d)} = 2 \times 10^8 \gg 1$

$$\mu = \frac{\varepsilon_c + \varepsilon_d}{2} + k_B T \ln \sqrt{\frac{N_d}{2N_c}} \quad \text{iž vaj}$$

$$\frac{\varepsilon_c - \mu}{k_B T} = \frac{\varepsilon_c - \varepsilon_d}{2} - \ln \sqrt{\frac{N_d}{2N_c}} = 9 \quad \begin{array}{l} \text{nedegeneriran} \\ \text{polprevodnik} \end{array}$$

$$N_c = \sqrt{\frac{N_d N_c}{2}} e^{-\beta \frac{\varepsilon_c - \varepsilon_d}{2}} = 1.4 \times 10^{11} / \text{cm}^3 \quad 1/2^+$$

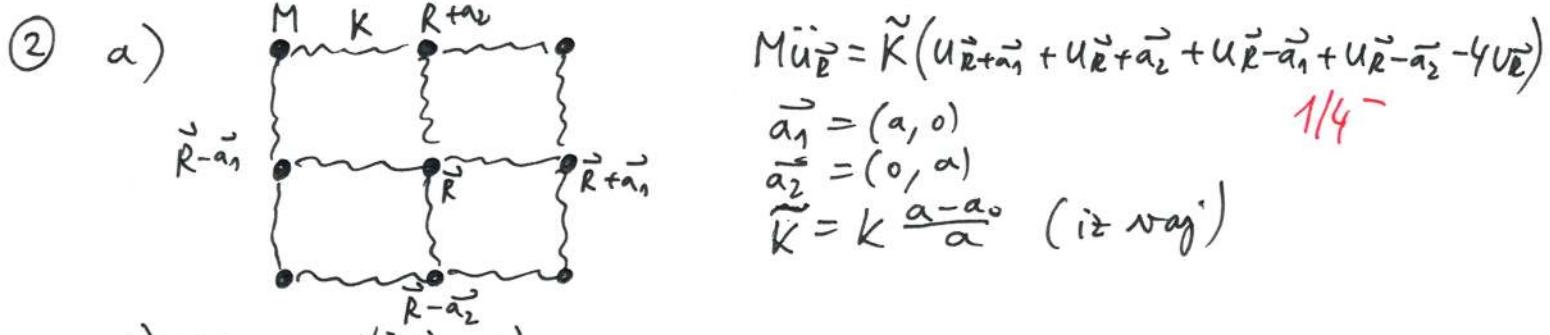
b) $T = 20 K \quad \frac{8N_d}{N_c} e^{\beta(\varepsilon_c - \varepsilon_d)} = 1.02$

$$\frac{\varepsilon_c - \mu}{k_B T} = \frac{\varepsilon_c - \varepsilon_d}{k_B T} - \ln \frac{-1 + \sqrt{1 + \frac{8N_d}{N_c} e^{\beta(\varepsilon_c - \varepsilon_d)}}}{4} = 4 \quad \begin{array}{l} \text{nedegeneriran} \\ \text{polprevodnik} \end{array}$$

$$N_c = N_c e^{-\beta(\varepsilon_c - \varepsilon_d)} \frac{-1 + \sqrt{1 + \frac{8N_d}{N_c} e^{\beta(\varepsilon_c - \varepsilon_d)}}}{4} = 8.3 \times 10^{14} / \text{cm}^3 \quad 1/2^-$$

Vzeli \approx valenčnem paru lahko zanemarimo, saj:

je $\frac{\varepsilon_c - \varepsilon_N}{k_B T} \approx 400$.



$$M\ddot{u}_R = \tilde{K}(u_R + \vec{a}_1 + u_R + \vec{a}_2 + u_R - \vec{a}_1 + u_R - \vec{a}_2 - 4u_R) \quad 1/4-$$

$$\vec{a}_1 = (\alpha, 0)$$

$$\vec{a}_2 = (0, \alpha)$$

$$\tilde{K} = K \frac{\alpha - \alpha_0}{\alpha} \text{ (is neg)}$$

b) $u_R = u_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$

$$-M\omega^2 u_0 = K(e^{i\vec{k} \cdot \vec{a}_1} + e^{i\vec{k} \cdot \vec{a}_2} + e^{-i\vec{k} \cdot \vec{a}_1} + e^{-i\vec{k} \cdot \vec{a}_2} - 4)u_0 =$$

$$= -4K(\sin^2 \frac{\vec{k} \cdot \vec{a}_1}{2} + \sin^2 \frac{\vec{k} \cdot \vec{a}_2}{2})$$

$$\omega = \sqrt{\frac{4K}{M} (\sin^2 \frac{\vec{k} \cdot \vec{a}_1}{2} + \sin^2 \frac{\vec{k} \cdot \vec{a}_2}{2})} \quad 1/4-$$

c) $|\vec{k}| \ll \frac{\pi}{a} \Rightarrow \omega = \sqrt{\frac{K}{M} k^2 a^2} \Rightarrow c = \sqrt{\frac{K}{M}} a \quad 1/4-$

d) $M\ddot{u}_R = \tilde{K}(u_R + \vec{a}_1 + u_R + \vec{a}_2 + u_R - \vec{a}_1 + u_R - \vec{a}_2 - 4u_R) + Q(v_R - u_R)$
 $M'\ddot{v}_R = \tilde{k}'(v_R + \vec{a}_1 + v_R + \vec{a}_2 + v_R - \vec{a}_1 + v_R - \vec{a}_2 - 4v_R) + Q(u_R - v_R)$
 $u_R = u_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$
 $v_R = v_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$
 $-M\omega^2 u_0 = \tilde{K}(-4\sin^2 \frac{\vec{k} \cdot \vec{a}_1}{2} - 4\sin^2 \frac{\vec{k} \cdot \vec{a}_2}{2})u_0 + Q(v_0 - u_0)$
 $-M'\omega^2 v_0 = \tilde{k}'(-4\sin^2 \frac{\vec{k} \cdot \vec{a}_1}{2} - 4\sin^2 \frac{\vec{k} \cdot \vec{a}_2}{2})v_0 + Q(u_0 - v_0)$
 $\det \begin{bmatrix} 4\tilde{K}(\sin^2 \frac{\vec{k} \cdot \vec{a}_1}{2} + \sin^2 \frac{\vec{k} \cdot \vec{a}_2}{2}) + Q - M\omega^2, & -Q \\ -Q, & 4\tilde{k}'(\sin^2 \frac{\vec{k} \cdot \vec{a}_1}{2} + \sin^2 \frac{\vec{k} \cdot \vec{a}_2}{2}) + Q - M'\omega^2 \end{bmatrix} = 0$
 $\vec{k} = 0 \Rightarrow (Q - M\omega^2)(Q - M'\omega^2) - Q^2 = 0$
 $-(n + n')Q\omega^2 + MM'\omega^4 = 0$
 $\omega_{opt} = \sqrt{Q \frac{n+n'}{MM'}} \quad 1/4-$

e) $|\vec{k}| \ll \frac{\pi}{a}:$ $\det \begin{bmatrix} \tilde{K}k^2 a^2 + Q - M\omega^2, & -Q \\ -Q, & \tilde{k}'k^2 a^2 + Q - M'\omega^2 \end{bmatrix} = 0$
 $\omega = c\vec{k}$
 $[Q + (\tilde{K}a^2 - Mc^2)\vec{k}^2] [Q + (\tilde{k}'a^2 - M'c^2)\vec{k}^2] - Q^2 = 0$
 $Q[(\tilde{K} + \tilde{k}')a^2 - (n + n')c^2]\vec{k}^2 + O(\vec{k}^4) = 0 \Rightarrow c = \sqrt{\frac{\tilde{K} + \tilde{k}'}{n + n'}} a \quad 1/4-$

f) Ta $Q=0$ imamo dve akustični regi s $c = \sqrt{\frac{K}{M}} a$ i $c' = \sqrt{\frac{K'}{M'}} a$. Izračunajmo majorij prispevok spodnje plasti:

$$c = \frac{1}{N} \frac{dE}{dT} \quad E = \sum_{\vec{k}} \frac{1}{\hbar} w_{\vec{k}} \frac{1}{e^{\beta w_{\vec{k}} - 1}} = \frac{Na^2}{(2\pi)^2} \int_0^{\infty} 2\pi k dk \frac{1}{e^{\beta ck} - 1}$$

$$\textcircled{2} \quad f) \quad E = \frac{Na^2}{2\pi} \int_0^\infty \frac{u^2 du}{e^{u-1}} \left(\frac{1}{(\hbar c)^2 \beta_B^3} \right)$$

$$C = \frac{\alpha^2}{2\pi} \frac{3k_B^3 T^2}{(\hbar c)^2} \cdot 2 \wp(3)$$

$$C = \frac{3\wp(3)}{\pi} \left(\frac{k_B T}{\hbar \sqrt{\frac{E}{N}}} \right)^2 k_B$$

zu obere plasti: $C = \frac{3\wp(3)}{\pi} \left[\left(\frac{k_B T}{\hbar \sqrt{\frac{E}{N}}} \right)^2 + \left(\frac{k_B T}{\hbar \sqrt{\frac{E}{N}}} \right)^2 \right] k_B \quad 1/4-$